Solving Ordinary Differential Equations using MATLAB

Initial Value Problems

The typical IVPs are "vector form first order explicit ODEs" given by

$$(IVP): \begin{cases} \dot{\vec{x}}(t) = \vec{f}(t, \vec{x}(t)), \\ \vec{x}(t_0) = \vec{x}_0 \end{cases}$$

where $\vec{x}^T(t) = [x_1(t), \ldots, x_n(t)]$ is the "state vector", $\vec{x}(t_0) = \vec{x}_0 = [x_1(t_0), \ldots, x_n(t_0)]^T$ is the initial value (state), and $\vec{f}^T = [f_1, \ldots, f_n]$ is a (possibly nonlinear) function. Here we will try to understand and solve numerically for $\vec{x}(t)$, $t \in [t_0, t_f]$, where t_f is referred to as the terminal time.

Given a "small" calculation step h, the LHS of IVP can be approximated by

$$\dot{\vec{x}}(t) \approx \frac{\vec{x}(t_0 + h) - \vec{x}(t_0)}{t_0 + h - t_0}$$

so that the approximate solution at $t_0 + h$ can be written as

$$\underbrace{\hat{\vec{x}}(t_0 + h)}_{\hat{\vec{x}}_1} = \underbrace{\vec{x}(t_0)}_{\vec{x}_0} + \underbrace{h\vec{f}(t_0, \vec{x}(t_0))}_{\vec{f}_0}.$$

Of course, this representation contains the error, and it should be written (more generally) as

$$\vec{x}(t_0 + h) = \hat{\vec{x}}(t_0 + h) + \vec{R}_0 = \vec{x}_0 + h\vec{f}(t_0, \vec{x}_0) + R_0$$

where R_0 is the approximation error.

Denoting the state vector at time t_k by $\vec{x}_k$, the "Euler's Algorithm" generates a new state vector

$$(EM): \quad \vec{x}_{k+1} = \vec{x}_k + h_k \vec{f}(t_k, \vec{x}_k) \quad , \quad k = 0, 1, \dots$$

at time $t_k + h_k$. Note that, here $\vec{x}_k$ represents the approximation for $\vec{x}(t_k)$ $\left\{\begin{array}{l}\text{without using the} \\ \text{"∧" symbol}\end{array}\right\}$

Runge-Kutta

Fourth-Order fixed-step Runge-Kutta (RK) algorithm, which is considered to be an effective and easy to implement algorithm. Four additional intermediate variables are introduced such that

$$(RK4)_{k's}: \quad \begin{aligned} \vec{k}_1 &= h \vec{f}(t_k, \vec{x}_k) \\ \vec{k}_2 &= h \vec{f}\left(t_k + \frac{h}{2}, \vec{x}_k + \frac{\vec{k}_1}{2}\right) \\ \vec{k}_3 &= h \vec{f}\left(t_k + \frac{h}{2}, \vec{x}_k + \frac{\vec{k}_2}{2}\right) \\ \vec{k}_4 &= h \vec{f}(t_k + h, \vec{x}_k + \vec{k}_3) \end{aligned}$$

where h is the fixed step-size; the state vector at the next step is calculated via

$$(RK4): \quad \vec{x}_{k+1} = \vec{x}_k + \frac{1}{6}\left(\vec{k}_1 + 2\vec{k}_2 + 2\vec{k}_3 + \vec{k}_4\right)$$

0				
1/2	1/2			
1/2	0	1/2		
1	0	0	1	
	1/6	1/3	1/3	1/6

$$\begin{array}{c|c} \alpha & \beta \\ \hline & \gamma^T \end{array} \quad \begin{array}{l}\text{Butcher} \\ \text{array}\end{array}$$

Runge-Kutta-Fehlberg

Assuming that the current step-size is h_k, the six intermediate variables $\vec{k}_i$ are evaluated by

$$\vec{k}_i = h_k \, \vec{f}\left(t_k + \alpha_i h_k \, , \, \vec{x}_k + \sum_{j=1}^{i-1} \beta_{ij} \vec{k}_j \right) , \quad i = 1, 2, .., 6$$

where t_k is the current time, and α_i & β_{ij} are parameters, referred to as Dormand-Prince pairs.

The state vector at the next step is obtained from

$$\vec{x}_{k+1} = \vec{x}_k + \sum_{i=1}^{6} \gamma_i \vec{k}_i$$

The algorithm is also known as the "4/5 Runge-Kutta-Fehlberg (RKF45)" algorithm. The coefficients $\alpha_i, \beta_{ij}, \gamma_i$ are given below (Butcher array):

α_i	β_{ij}				
0					
1/4	1/4				
3/8	3/32	9/32	—		
12/13	1932/2197	−7200/2197	7296/2197		
1	439/216	−8	3680/513	−845/4104	
1/2	−8/27	2	−3544/2565	1859/4104	−11/40
γ_i	16/135	0	6656/12825	28561/56430	−9/50	2/5
$\rightarrow \gamma_i^*$	25/216	0	1408/2565	2197/4104	−1/5	0

Although the RKF45 seems to be a fixed-step size algorithm, in practical applications, an error vector

$$\vec{\epsilon}_k = \sum_{i=1}^{6} (\gamma_i - \gamma_i^*) \vec{k}_i$$

can be calculated, and accordingly the step-size h_k can be adjusted. Such an algorithm is known as "adaptive step-size" algorithm.
(variable)

Other RK Methods

General form of a third-order RK method is

$$\vec{k}_1 = h\vec{f}(t_i, \vec{z}_i)$$

$$\vec{k}_2 = h\vec{f}(t_i + \alpha_2 h, \vec{z}_i + \beta_{21}\vec{k}_1)$$

$$\vec{k}_3 = h\vec{f}(t_i + \alpha_3 h, \vec{z}_i + \beta_{31}\vec{k}_1 + \beta_{32}\vec{k}_2)$$

$$\vec{x}_{i+1} = \vec{z}_i + \gamma_1\vec{k}_1 + \gamma_2\vec{k}_2 + \gamma_3\vec{k}_3$$

0			
α_2	β_{21}		
α_3	β_{31}	β_{32}	
	γ_1	γ_2	γ_3

— RK3 Kutta's Method

0			
1/2	1/2		
1	−1	2	
	1/6	2/3	1/6

— RK3 Optimal Method

0			
1/2	1/2		
3/4	0	3/4	
	2/9	3/9	4/9

— RK3 Two-Thirds Rule

0			
2/3	2/3		
2/3	1/3	1/3	
	1/4	0	3/4

Multi-Step Methods

General (k-step) multistep method has the form

$$\vec{x}_{i+1} = \sum_{j=1}^{k} a_j \vec{x}_{i-j+1} + h \sum_{j=0}^{k} b_j \vec{f}_{i-j+1}$$

when $b_0 \neq 0$, the method is implicit; otherwise explicit.

Two common methods are derived from

— Adams (Multi-step) Methods

$$\vec{x}_{i+1} = \vec{x}_i + h \sum_{j=0}^{k} b_j \vec{f}_{i-j+1}$$

1°) Adams-Bashforth
   when $b_0 = 0$ (explicit)

2°) Adams-Moulton
   when $b_0 \neq 0$ (implicit).

Eg: Third-Order Adams-Bashforth:

$$\vec{x}_{i+1} = \vec{x}_i + \frac{h}{12} \left[23 \vec{f}_i - 16 \vec{f}_{i-1} + 5 \vec{f}_{i-2} \right]$$

Eg: Third-Order Adams-Moulton:

$$\vec{x}_{i+1} = \vec{x}_i + \frac{h}{12} \left[5 \vec{f}_{i+1} + 8 \vec{f}_i - \vec{f}_{i-1} \right]$$

Predictor – Corrector Methods

Eg: ABM3:

$$\vec{x}_{i+1}^{\,*} = \vec{x}_i + \frac{h}{12}\left[23\vec{f}_i - 16\vec{f}_{i-1} + 5\vec{f}_{i-2}\right]$$

$$\vec{x}_{i+1} = \vec{x}_i + \frac{h}{12}\left[5\vec{f}_{i+1}^{\,*} + 8\vec{f}_i - \vec{f}_{i-1}\right]$$

Note that initially a one-step method, such as RK3 (variant), should be used to compute $\vec{x}_1$ and $\vec{x}_2$, besides $\vec{x}_0$.

BDF (Backward Differentiation Formula) Methods

Such methods arise from

$$\dot{\vec{x}}_{i+1} = \vec{f}(t_{i+1}, \vec{x}_{i+1})$$

with $\dot{\vec{x}}_{i+1}$ is replaced by a backward difference formula, $\quad \dfrac{\vec{x}_{i+1} - \vec{x}_i}{h}$.

BDF k-Step Methods has a general form

$$\vec{x}_{i+1} = \sum_{j=1}^{k} a_j \, \vec{x}_{i-j} + b_0 \, h \, \vec{f}_{i+1}$$
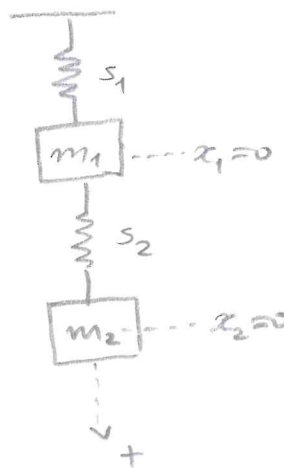
Mass-Spring System

$$m_1 x_1'' = -S_1 x_1 + S_2(x_2 - x_1)$$

$$m_2 x_2'' = -S_2(x_2 - x_1)$$

$$m_1 = 10, \quad m_2 = 2$$
$$S_1 = 100, \quad S_2 = 120$$

$$x_1(0) = \tfrac{1}{2} \qquad x_1'(0) = 0$$
$$x_2(0) = \tfrac{1}{4} \qquad x_2'(0) = 0$$

Converted to system as follows, $u_1 = x_1$, $u_2 = x_1'$,
$u_3 = x_2$, $u_4 = x_2'$

$$u_1' = u_2$$

$$u_2' = -\frac{S_1}{m_1} u_1 + \frac{S_2}{m_1}(u_3 - u_1)$$

$$u_3 = u_4$$

$$u_4 = -\frac{S_2}{m_2}(u_3 - u_1)$$

$$\vec{u}(0) = \begin{bmatrix} 1/2 \\ 0 \\ 1/4 \\ 0 \end{bmatrix}$$

Lorenz Equation.

$$\dot{x}_1(t) = -\beta x_1(t) + x_2(t) x_3(t)$$

$$\dot{x}_2(t) = -\rho x_2(t) + \rho x_3(t)$$

$$\dot{x}_3(t) = -x_1(t) x_2(t) + \sigma x_2(t) - x_3(t)$$

where $\beta = 8/3$, $\rho = 10$, $\sigma = 28$. Let the initial state
be $x_1(0) = x_2(0) = 0$, $x_3(0) = \epsilon$ (small; $\epsilon = 10^{-10}$).

Van der Pol Equation

$$\ddot{y} + \mu(y^2 - 1)\dot{y} + y = 0$$

$$y(0) = -0.2, \quad \dot{y}(0) = -0.7$$

μ is a parameter
such as $\mu = 1$ or $\mu = 2$.
(thus take $\mu = 1000$)

Satellite Equation

$$\ddot{x} = 2\dot{y} + x - \frac{\mu^*(x+\mu)}{r_1^3} - \frac{\mu(x-\mu^*)}{r_2^3},$$

$$\ddot{y} = -2\dot{x} + y - \frac{\mu^* y}{r_1^3} - \frac{\mu y}{r_2^3}$$

where $\mu = \frac{1}{82.45}$, $\mu^* = 1 - \mu$, $r_1 = \sqrt{(x+\mu)^2 + y^2}$
$r_2 = \sqrt{(x-\mu^*)^2 + y^2}$. Let the initial conditions be

$$x(0) = 1.2 \qquad y(0) = 0$$

$$\dot{x}(0) = 0 \qquad \dot{y}(0) = -1.04935751.$$

Stiff Equations

$$\dot{y} = \begin{bmatrix} -21 & 19 & -20 \\ 19 & -21 & 20 \\ 40 & -40 & -40 \end{bmatrix} y, \quad y_0 = \begin{bmatrix} 1 \\ 0 \\ -1 \end{bmatrix}$$

with the exact solution

$$y(t) = \begin{bmatrix} 0.5\,e^{-2t} + 0.5\,e^{-40t}(\cos 40t + \sin 40t) \\ 0.5\,e^{-2t} - 0.5\,e^{-40t}(\cos 40t + \sin 40t) \\ e^{-40t}(\sin 40t - \cos 40t) \end{bmatrix}$$

Implicit Equations

$$\begin{cases} (\sin x_1)\,\dot{x}_1 + (\cos x_2)\,\dot{x}_2 + x_1 = 1 \\ (-\cos x_2)\,\dot{x}_1 + (\sin x_1)\,\dot{x}_2 + x_2 = 0 \end{cases}$$

Equivalently, for $\vec{x} = [x_1, x_2]^T$,

$$A(\vec{x})\,\dot{\vec{x}} = B(\vec{x}), \quad A(\vec{x}) = \begin{bmatrix} \sin x_1 & \cos x_2 \\ -\cos x_2 & \sin x_1 \end{bmatrix} \text{ is non-singular}$$

OR $\dot{\vec{x}} = A^{-1}(\vec{x})\,B(\vec{x})$ $\qquad B(\vec{x}) = \begin{bmatrix} 1 - x_1 \\ -x_2 \end{bmatrix}$

OR Really Implicit Equation

$$\begin{cases} \ddot{x}\sin\dot{y} + \ddot{y}^2 = -2xy\,e^{-\dot{x}} + x\ddot{x}\dot{y} \\ x\ddot{x}\ddot{y} + \cos\ddot{y} = 3y\dot{x}e^{-x} \end{cases}$$

Equivalently, letting $x_1 = x$, $x_2 = \dot{x}$, $x_3 = y$, $x_4 = \dot{y}$
and denoting $p_1 = \ddot{x}$ and $p_2 = \ddot{y}$ we have

$$\begin{cases} p_1\sin x_4 + p_2^2 + 2x_1 x_3\,e^{-x_2} - x_1 p_1 x_4 = 0 \\ x_1 p_1 p_2 + \cos p_2 - 3x_3 x_2\,e^{-x_1} = 0. \end{cases}$$

Let the initial state be $[x_1, x_2, x_3, x_4] = [1, 0, 0, 1]$
$\qquad\qquad\qquad\qquad\qquad \underset{x}{1} \ \underset{\dot{x}}{1} \ \underset{y}{1} \ \underset{\dot{y}}{1} \Big|_{t=0}$